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## Physics and Chemistry of Liquids

Publication details, including instructions for authors and subscription information:

<http://www.informaworld.com/smpp/title~content=t713646857>

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**To cite this Article** Hua, Li and Wanren, Chen(2006) 'Solubility of dilute SO<sub>2</sub> in DMSO Mn<sup>2</sup> mixture solvents and EOS model-(II)', *Physics and Chemistry of Liquids*, 44: 1, 83 – 93

**To link to this Article:** DOI: 10.1080/00319100500381508

**URL:** <http://dx.doi.org/10.1080/00319100500381508>

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## Solubility of dilute SO<sub>2</sub> in DMSO + Mn<sup>2+</sup> mixture solvents and EOS model-(II)

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(Received 15 August 2005)

On the basis of solubility measurement of dilute SO<sub>2</sub> in DMSO + Mn<sup>2+</sup> mixture solvents, a new EOS model was established to represent gas–liquid equilibrium system, and the solubilities calculated by the model show good agreement with experimental data.

*Keywords:* Solubility; Gas–liquid equilibrium; Sulfur dioxide; EOS

### 1. Introduction

On the basis of solubility measurement of dilute SO<sub>2</sub> in DMSO + Mn<sup>2+</sup> mixture solvents, we established an EOS model based on experimental data. This model is set out in detail in section 2 immediately below. A summary is presented in section 3.

### 2. The EOS model

In the literature, the various models used to obtain a representation of gas in electrolyte solution systems may be divided into three kinds of approaches: The first one corresponds to empirical treatments. However, its extrapolation capabilities are weak. The second approach is based on an excess Gibbs energy model. In the last kind of approach, equations of state are used. The EOS approach is better than other approaches, because the same reference states were adopted for liquid and gas phases, on Henry constants being needed in this case. Furthermore, the EOS approach is more simple and practical than the excess Gibbs energy model, for some systems that haven't the excess Gibbs energy expression, it can be represented by the EOS.

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Therefore in this study, on the basis of the EOS derived by Furst [1], a new EOS model has been established to represent gas–liquid equilibrium.

### 2.1. The expression of Helmholtz energy for electrolyte solution

In this model the molar of Helmholtz energy is developed as the sum of four contributions, considering interaction energy between ions and solvent and between cations and anions on the basis of EOS derived by Furst *et al.* [1–7]

$$\left(\frac{\Delta A}{RT}\right) = \left(\frac{\Delta A}{RT}\right)_{RF} + \left(\frac{\Delta A}{RT}\right)_{SR1} + \left(\frac{\Delta A}{RT}\right)_{SR2} + \left(\frac{\Delta A}{RT}\right)_{LR}. \quad (1)$$

The first term (RF) is relative to repulsive forces, the second one (SR1) represents attractive short-range interactions involving no ions. The third one (SR2) represents solvation interactions between ions and molecules or between cations and anions. The last term (LR) is the long-range electrostatic interaction contribution.

**2.1.1. The Helmholtz energy arising from the repulsive forces.** This can be expressed through the improved SRK equation of state given by Wang [8,9]

$$\left(\frac{\Delta A}{RT}\right)_{RF} = \sum_k x_k \ln \frac{x_k RT}{p_0(v-b)}. \quad (2)$$

**2.1.2. The Helmholtz energy arising from the attractive forces.** This can be expressed through the improved SRK equation of state by Wang [8,9]:

$$\left(\frac{\Delta A}{RT}\right)_{SR1} = \frac{a^{SR}}{bRT} \ln \frac{v}{v+b} \quad (3)$$

$$b = b_m + \sum_{i=ion} x_i b_i \quad (4)$$

$$b_i \text{ is defined by: } b_i = N\pi\sigma_i^3/6 \quad (5)$$

where  $N$  is Avogadro's number,  $\sigma$  is the hard-sphere diameter, relevant data being shown in table 4. For the molecular mixture, the parameters are calculated using the Wong-Sandler mixing rule [10,11].

$$b_m = \left[ \sum_n \sum_m x_n x_m \left( b - \frac{a^{SR}}{RT} \right)_{nm} \right] / \left[ 1 + \left( \frac{A_\infty^E(x)}{RT} \right) - \sum_n x_n \left( \frac{a_n}{b_n RT} \right) \right] \quad (6)$$

$$\left( b - \frac{a^{SR}}{RT} \right)_{nm} = \left[ \left( b_n - \left( \frac{a_n^{SR}}{RT} \right) \right) + \left( b_m - \left( \frac{a_m^{SR}}{RT} \right) \right) \right] / 2(1 - k_{nm}) \quad (7)$$

where (7)  $k_{nm}$  is the binary parameter which can be calculated from critical constants [12]. In equation (6), another term is calculated from

$$\frac{A_{\infty}^E}{RT} = \sum_n x_n \left( \frac{\sum_m x_m \tau_{nm} g_{nm}}{\sum_m x_m g_{nm}} \right) \quad (8)$$

where (8),

$$g_{nm} = \exp(-0.3\tau_{nm}) \quad (9)$$

the binary parameters  $\tau_{nm}$  are obtained by fitting gas solubility data at various temperatures and pressures, and these are shown in table 3.

The parameter  $a^{SR}$  is calculated as follows,

$$a^{SR} = b_m \left( \sum_n x_n \frac{a_n^{SR}}{b_n} - A_{\infty}^E(x) \right). \quad (10)$$

The pure molecular components attractive parameter  $a_n^{SR}$  is calculated using the expression presented by the improved SRK equation of state by Wang [8,9]

$$a_n^{SR} = 0.42748 \frac{(RT_c)^2}{p_c} \left[ 1 + m_1(1 - \sqrt{T_r}) + m_2(1 - \sqrt{T_r})^2 + m_3(1 - \sqrt{T_r})^3 \right]^2 \quad \text{for } T_r \leq 1 \quad (11)$$

$$a_n^{SR} = 0.42748 \frac{(RT_c)^2}{p_c} \left[ 1 + m_1(1 - \sqrt{T_r}) \right]^2 \quad \text{for } T_r > 1 \quad (12)$$

where,

$$m_1 = 0.48344 + 1.58597\omega - 0.3758\omega^2 + 0.23194\omega^3 \quad (13)$$

$$m_2 = 0 \quad (0.35 < \omega \leq 0.56) \quad (14)$$

$$m_3 = 25.689 - 108.63\omega + 150.68\omega^2 - 68.739\omega^3 \quad (\omega > 0.56). \quad (15)$$

for the SO<sub>2</sub>, DMSO,  $m_1$  is calculated by equation (13). The values of pure molecular component parameters are listed in table 2.

**2.1.3. The term of short-range forces to the Helmholtz energy.** The third term of the Helmholtz energy expression takes into account interactions between ions and molecules or between cations and anions. This contribution may be considered as the solvation contribution.

$$\left( \frac{\Delta A}{RT} \right)_{SR_2} = \sum_k \sum_l \frac{x_k x_l W_{kl}}{v(1 - \zeta_3)} \quad (16)$$

in which (16), at least one of  $k$  and  $l$  is an ion, and the packing factor  $\zeta_3$  is defined as,

$$\zeta_3 = \frac{N\pi}{6} \sum_k \frac{x_k \sigma_k^3}{v} \quad (17)$$

$\sigma_k$  is the diameter of a molecular or an ion, the data is shown in table 4,  $W_{kl}$  is an adjustable parameter.

**2.1.4. The term of long-range forces to the Helmholtz energy.** The last term of the Helmholtz energy expression is the long-range electrostatic interaction contribution that is represented with a simplified MSA model proposed by Ball *et al.* [17]:

$$\left(\frac{\Delta A}{RT}\right)_{LR} = -\frac{\alpha_{LR}^2}{4\pi} \sum_i \frac{x_i Z_i^2 \Gamma}{1 + \Gamma \sigma_i} + \frac{v\Gamma^3}{3\pi N} \quad (18)$$

where the shielding parameter  $\Gamma$  is obtained from the following relations [16]:

$$\Gamma = \frac{\alpha_{LR}}{2} \left[ \rho \sum_{j=1}^c x_j (z_j + \sigma_j f_j)^2 \right]^{1/2} \quad (19)$$

$$\text{where: } f_j = \frac{\pi C'}{4B'} - \frac{z_j(\alpha_{LR}/2)A' + (\pi\alpha_{LR}A'E')/(12B')}{D'} \quad (20)$$

$$A' = \left( \rho \sum_{i=1}^c x_i z_i^2 \right)^{1/2} \quad (21)$$

$$B' = \left( 1 - \frac{\pi}{6} \rho \sum_{i=1}^c x_i \sigma_i^3 \right) \quad (22)$$

$$C' = \rho \sum_{i=1}^c x_i z_i \sigma_i^2 \quad (23)$$

$$D' = 1 + \alpha_{LR} \left( \rho \sum_{i=1}^c x_i z_i^2 \sigma_i^2 \right)^{1/2} \quad (24)$$

$$E' = \rho \sum_{i=1}^c x_i \sigma_i^3 z_i. \quad (25)$$

Here  $\rho$  is number density of total particle in this system, and is defined by:

$$\rho = \rho_m + \rho_i. \quad (26)$$

Also  $\alpha_{LR}$  can be calculated as:

$$\alpha_{LR}^2 = \frac{\varepsilon^2 N}{\varepsilon_0 D R T} \quad (27)$$

where  $e$  is protonic charge ( $1.60219 \times 10^{-19}$  C);  $\varepsilon_0$  is electric permittivity of freespace ( $8.45188 \times 10^{-12}$  J<sup>-2</sup> C<sup>-2</sup> m<sup>-1</sup>). In equation (27),  $D$  is dielectric constant of the solution, which takes into account the influence of the ions through Pottel's expression [18]:

$$D = 1 + (D_s - 1) \left( \frac{1 - \xi_3}{1 + \xi_3/2} \right) \quad (28)$$

where  $D_s$  is the solvent dielectric constant. In turn this is deduced from the various molecular contributions  $D_m$  by

$$D_s = \frac{\sum_m x_m D_m}{\sum_m x_m}. \quad (29)$$

In equation (28),  $\xi_3$  is defined by equation (17).

Through analysis of the four terms on the RHS of equation (1), only two types of parameters appear in above-mentioned equation, one is a critical parameter and hard-sphere diameter, these being obtained from the literature; another type consists of binary interaction parameters from experimental solubilities. Finally, the calculated parameter is optimized  $W_{kl}$  parameters for binary systems.

## 2.2. The equations of state of electrolyte solution

From thermodynamics we have,

$$dA = -SdT - PdV \quad (30)$$

at constant temperature,

$$P = -\left(\frac{\partial A}{\partial V}\right)_{T, n_k}. \quad (31)$$

Substituting equation (1) and other expressions in equation (31), the equation of state of electrolyte solution is deduced as

$$\left(\frac{P}{RT}\right) = \left(\frac{P}{RT}\right)_{RF} + \left(\frac{P}{RT}\right)_{SR1} + \left(\frac{P}{RT}\right)_{SR2} + \left(\frac{P}{RT}\right)_{LR} \quad (32)$$

where

$$\left(\frac{P}{RT}\right)_{RF} = \frac{1}{v - b} \quad (33)$$

$$\left(\frac{P}{RT}\right)_{SR1} = \frac{a^{SR}}{RTv(v + b)} \quad (34)$$

$$\left(\frac{P}{RT}\right)_{SR2} = -\sum_k \sum_l \frac{x_k x_l W_{kl}}{v^2(1 - \zeta_3)^2} \quad (35)$$

$$\left(\frac{P}{RT}\right)_{LR} = -\frac{\alpha_{LR}^2}{4\pi D} \left(\frac{\partial D}{\partial V}\right)_{T, n_k} \sum_j \frac{n_j Z_j^2 \Gamma}{1 + \Gamma \sigma_j} - \frac{\Gamma^3}{3\pi N}. \quad (36)$$

For the molecular mixtures, the parameters are calculated using the Wong-Sandler mixing rule.

### 2.3. The calculation of gas–liquid phase equilibrium

On the EOS of the system under consideration, one can write the fugacity coefficient expression given by Prausnitz [19] as:

$$\ln \hat{\phi}_i = \frac{1}{RT} \int_v^\infty \left[ \left( \frac{\partial P}{\partial n_i} \right)_{T, V, n_j} - \frac{RT}{V} \right] dV - \ln Z. \quad (37)$$

The fugacity coefficient for gas–liquid equilibrium can be calculated by the differential and integral method, further calculating phase equilibrium properties of the electrolyte solution according to the fundamental thermodynamic relationship for gas–liquid equilibrium

$$y_i \hat{\phi}_i^g = x_i \hat{\phi}_i^L \quad (38)$$

where the representation of the component is such that subscript 0 represents  $\text{SO}_2$ , 1 represents DMSO, 2 represents  $\text{Mn}^{2+}$ , 3 represents  $\text{SO}_4^{2-}$ , 4 represents  $\text{H}^+$ . Therefore the specific expression is:

$$b = b_m + x_2 b_2 + x_3 b_3 + x_4 b_4 \quad (39)$$

where  $b_m$  represents the parameter for the molecular mixtures,  $b_2, b_3, b_4$  represents the parameter for the ions in the solution.

The ionic covolumes  $b_i$  are deduced from equation (5).

The molecular mixture covolumes  $b_m$  can be calculated by:

$$b_m = \left[ 2x_0 x_1 \left( b - \frac{a}{RT} \right)_{01} + x_0^2 \left( b - \frac{a}{RT} \right)_{00} + x_1^2 \left( b - \frac{a}{RT} \right)_{11} \right] / \left[ 1 - \left( x_1 \frac{a_1}{b_1 RT} + x_0 \frac{a_0}{b_0 RT} \right) + \frac{A_\infty^E}{RT} \right] \quad (40)$$

where,

$$\frac{A_\infty^E}{RT} = \frac{x_0(x_0 \tau_{00} g_{00} + x_1 \tau_{10} g_{10})}{x_0 g_{00} + x_1 g_{10}} + \frac{x_1(x_0 \tau_{01} g_{01} + x_1 \tau_{11} g_{11})}{x_0 g_{01} + x_1 g_{11}} \quad (41)$$

due to the binary parameters  $g_{ii} = g_{jj} = 1$ ,  $\tau_{ii} = \tau_{jj} = 0$ , so equation (41) can be simplified as:

$$\frac{A_\infty^E}{RT} = \frac{x_0 x_1 \tau_{10} g_{10}}{x_0 + x_1 g_{10}} + \frac{x_1 x_0 \tau_{01} g_{01}}{x_0 g_{01} + x_1} \quad (42)$$

$g_{nm}$  can be calculated as equation (9) the parameters of  $\tau_{10}$  and  $\tau_{01}$  are obtained by fitting gas solubility data at various temperatures and partial pressures. The regressed binary parameters for the binary systems are listed in table 3,  $(b - (a^{SR}/(SR)))_{nm}$  can be calculated as in equation (7). The hard-sphere diameter  $\sigma$  of DMSO is calculated

by Ried [15],  $\sigma = 0.809V_c^{1/3}$ ,  $V_c$  is the critical volume (122.2 cm<sup>3</sup>/mol). The calculated result is listed in table 4.

In this system,  $a_n^{SR}$  is calculated by:

$$a^{SR} = b_m \left( \frac{x_1 a_1^{SR}}{b_1} + \frac{x_2 a_2^{SR}}{b_2} - A_\infty^E \right) \quad (43)$$

$$\zeta_3 = \frac{N \times 3.14 x_0 \sigma_0^3 + x_1 \sigma_1^3 + x_2 \sigma_2^3 + x_3 \sigma_3^3 + x_4 \sigma_4^3}{6v} \quad (44)$$

while  $a_{LR}$  can be calculated as equation (27).

$D$  can be calculated following equation (28) using

$$D_s = \frac{x_0 D_0 + x_1 D_1}{x_0 + x_1} \quad (45)$$

The dielectric constants for SO<sub>2</sub> DMSO are listed in table 5.

This model relates to 5 components of SO<sub>2</sub>, DMSO, Mn<sup>2+</sup>, SO<sub>4</sub><sup>2-</sup>, H<sup>+</sup>, and contains 6 adjustable parameters  $W_{kl}$ . As in previous works (Li [20, 21]), in this study we have used a similar approach, ignored the  $W_{24}$ ,  $W_{03}$ ,  $W_{13}$  parameters because of the well-known charge repulsion effect and because the solvation is generally lower in the case of anions if compared to cations. Hence the model only involved six adjustable parameters  $W_{cm}$  and  $W_{ca}$  between cation (c) and molecule (m), cation and anion (a).

Furthermore the interaction parameters  $W_{43}$  and  $W_{32}$  could also be related to  $\sigma_c^s$  and  $\sigma_a^p$  by equation (5) and

$$W_{ca} = \lambda_5(\sigma_c^s + \sigma_a^p)^4 + \lambda_6. \quad (46)$$

In these correlations, Stokes diameter  $\sigma_c^s$  for the cations and anionic Pauling diameter  $\sigma_a^p$  for the anions are involved. The values of Pauling and Stokes diameters are listed in table 4. In these correlations the ionic diameters are expressed in Angstroms, the values of coefficients  $\lambda_5$ ,  $\lambda_6$  being  $-0.03208 \times 10^{-6}$ ,  $18.93 \times 10^{-6}$  respectively, these values were from literature [1]. By equation (46), we can obtain,  $W_{43} = -7.92 \times 10^{-4}$  m<sup>3</sup>/mol,  $W_{32} = -3.85 \times 10^{-4}$  m<sup>3</sup>/mol. So experimental data determines four adjustable parameters (table 5).

#### 2.4. Optimization calculation

By experimental data correlation, 4 interaction parameters are obtained. They are

$$\begin{aligned} W_{40} &= 0.00152 \text{ m}^3/\text{mol}, & W_{41} &= 0.132 \text{ m}^3/\text{mol} \\ W_{20} &= -7.63 \text{ m}^3/\text{mol}, & W_{21} &= 1.51 \times 10^2 \text{ m}^3/\text{mol} \end{aligned}$$

The comparison between calculated results according to these parameters and experimental data is summarized in table 1. The comparison of SO<sub>2</sub> solubilities calculated by the model and experimental data at different SO<sub>2</sub> partial pressures are shown in figure 1. Obviously, the solubilities calculated by the model are in good agreement with the experimental data.



Table 1. The comparison of experimental data and calculation values for SO<sub>2</sub> solubilities in mixture absorbent.

| $T$ (K) | $P_{\text{SO}_2}$ , kPa | $x_{\text{H}_2\text{SO}_4}$ | $x_{\text{MnSO}_4}$ | $x_{\text{DMSO}}$ | $y_{\text{SO}_2}$ | $y_{\text{O}_2}$ | $y_{\text{DMSO}}$ | $y_{\text{N}_2}$ | $x_{\text{SO}_2}$ |                  |
|---------|-------------------------|-----------------------------|---------------------|-------------------|-------------------|------------------|-------------------|------------------|-------------------|------------------|
|         |                         |                             |                     |                   |                   |                  |                   |                  | $x_{\text{exp}}$  | $x_{\text{cal}}$ |
| 294.15  | 0.228                   | 0.0366                      | 0.00195             | 0.943             | 0.00229           | 0.0776           | 0.00183           | 0.918            | 0.0185            | 0.0197           |
| 294.15  | 0.306                   | 0.0478                      | 0.00191             | 0.925             | 0.00307           | 0.116            | 0.00183           | 0.879            | 0.0253            | 0.0238           |
| 294.15  | 0.585                   | 0.0563                      | 0.00187             | 0.903             | 0.00585           | 0.187            | 0.00182           | 0.806            | 0.0387            | 0.0382           |
| 294.15  | 0.865                   | 0.0644                      | 0.00182             | 0.882             | 0.00862           | 0.257            | 0.00181           | 0.733            | 0.0516            | 0.0521           |
| 294.15  | 0.956                   | 0.0824                      | 0.00178             | 0.860             | 0.00949           | 0.271            | 0.00181           | 0.718            | 0.056             | 0.0565           |
| 294.15  | 1.450                   | 0.0975                      | 0.00170             | 0.821             | 0.0144            | 0.321            | 0.00180           | 0.663            | 0.0798            | 0.0796           |
| 294.15  | 1.945                   | 0.111                       | 0.00162             | 0.786             | 0.0194            | 0.386            | 0.00180           | 0.593            | 0.101             | 0.102            |
| 298.15  | 0.227                   | 0.0377                      | 0.00195             | 0.943             | 0.00228           | 0.0775           | 0.00260           | 0.918            | 0.0175            | 0.0185           |
| 298.15  | 0.303                   | 0.0496                      | 0.00191             | 0.925             | 0.00304           | 0.116            | 0.00260           | 0.878            | 0.0238            | 0.0224           |
| 298.15  | 0.582                   | 0.0575                      | 0.00187             | 0.904             | 0.00582           | 0.186            | 0.00259           | 0.805            | 0.0366            | 0.0365           |
| 298.15  | 0.861                   | 0.0649                      | 0.00183             | 0.884             | 0.00859           | 0.256            | 0.00258           | 0.733            | 0.0488            | 0.0497           |
| 298.15  | 0.902                   | 0.1009                      | 0.00175             | 0.845             | 0.00859           | 0.270            | 0.00256           | 0.718            | 0.0519            | 0.0516           |
| 298.15  | 1.422                   | 0.1141                      | 0.00167             | 0.810             | 0.0142            | 0.320            | 0.00256           | 0.663            | 0.0743            | 0.0742           |
| 298.15  | 1.941                   | 0.1261                      | 0.00161             | 0.777             | 0.0194            | 0.385            | 0.00256           | 0.593            | 0.0948            | 0.0949           |
| 303.15  | 0.223                   | 0.0427                      | 0.00194             | 0.939             | 0.00223           | 0.0774           | 0.00364           | 0.917            | 0.0159            | 0.0171           |
| 303.15  | 0.298                   | 0.0524                      | 0.00191             | 0.924             | 0.00297           | 0.116            | 0.00362           | 0.878            | 0.0217            | 0.0208           |
| 303.15  | 0.542                   | 0.0705                      | 0.00185             | 0.895             | 0.00541           | 0.186            | 0.00362           | 0.805            | 0.0331            | 0.0323           |
| 303.15  | 0.787                   | 0.0875                      | 0.00179             | 0.867             | 0.00786           | 0.256            | 0.00362           | 0.733            | 0.0437            | 0.0431           |
| 303.15  | 0.900                   | 0.1108                      | 0.00174             | 0.840             | 0.00893           | 0.270            | 0.00361           | 0.718            | 0.0472            | 0.0478           |
| 303.15  | 1.421                   | 0.1229                      | 0.00167             | 0.808             | 0.0142            | 0.320            | 0.00360           | 0.662            | 0.0677            | 0.0684           |
| 303.15  | 1.943                   | 0.1340                      | 0.00161             | 0.7769            | 0.0194            | 0.385            | 0.00365           | 0.592            | 0.0875            | 0.0871           |
| 308.15  | 0.186                   | 0.0483                      | 0.00193             | 0.936             | 0.00186           | 0.0771           | 0.00504           | 0.916            | 0.0142            | 0.0148           |
| 308.15  | 0.290                   | 0.0597                      | 0.00190             | 0.919             | 0.00289           | 0.116            | 0.00502           | 0.876            | 0.0194            | 0.0193           |
| 308.15  | 0.518                   | 0.0813                      | 0.00183             | 0.888             | 0.00517           | 0.186            | 0.00503           | 0.804            | 0.0294            | 0.0287           |
| 308.15  | 0.746                   | 0.1014                      | 0.00177             | 0.858             | 0.00745           | 0.256            | 0.00502           | 0.732            | 0.0388            | 0.0376           |
| 308.15  | 0.895                   | 0.125                       | 0.00172             | 0.832             | 0.00889           | 0.270            | 0.00502           | 0.717            | 0.0419            | 0.0432           |
| 308.15  | 1.377                   | 0.148                       | 0.00164             | 0.791             | 0.0137            | 0.319            | 0.00501           | 0.662            | 0.0595            | 0.0599           |
| 308.15  | 1.858                   | 0.169                       | 0.00156             | 0.754             | 0.0185            | 0.384            | 0.00501           | 0.592            | 0.0754            | 0.0751           |
| 313.15  | 0.182                   | 0.0519                      | 0.00193             | 0.935             | 0.00182           | 0.0769           | 0.00690           | 0.914            | 0.0115            | 0.0118           |
| 313.15  | 0.271                   | 0.0685                      | 0.00189             | 0.914             | 0.00270           | 0.115            | 0.00689           | 0.875            | 0.0159            | 0.0154           |
| 313.15  | 0.509                   | 0.0975                      | 0.00181             | 0.877             | 0.00507           | 0.185            | 0.00689           | 0.803            | 0.0236            | 0.024            |
| 313.15  | 0.719                   | 0.124                       | 0.00174             | 0.843             | 0.00718           | 0.255            | 0.00689           | 0.731            | 0.031             | 0.0309           |
| 313.15  | 0.798                   | 0.145                       | 0.00169             | 0.820             | 0.00794           | 0.269            | 0.00687           | 0.716            | 0.0336            | 0.0333           |
| 313.15  | 1.34                    | 0.168                       | 0.00162             | 0.783             | 0.0133            | 0.318            | 0.00686           | 0.662            | 0.0479            | 0.0481           |
| 313.15  | 1.88                    | 0.189                       | 0.00155             | 0.749             | 0.0187            | 0.383            | 0.00686           | 0.591            | 0.0609            | 0.0608           |

Table 2. The values of pure molecular component properties and parameters.

| Solvent     | DMSO                        | SO <sub>2</sub> |
|-------------|-----------------------------|-----------------|
| $T_c$ (K)   | 707 [13,14]                 | 430.8 [15]      |
| $P_c$ (kPa) | 5850 [13,14]                | 7880 [15]       |
| $\omega$    | 0.414 [13,14]               | 0.256 [15]      |
| $m_1$       | Calculated by equation (13) |                 |
| $m_2$       | 0 [15]                      | -1.9446 [8]     |
| $m_3$       | 0 [15]                      | 15.2851 [15]    |

Table 3. Optimized  $\tau_{ij}$  parameters for binary systems.

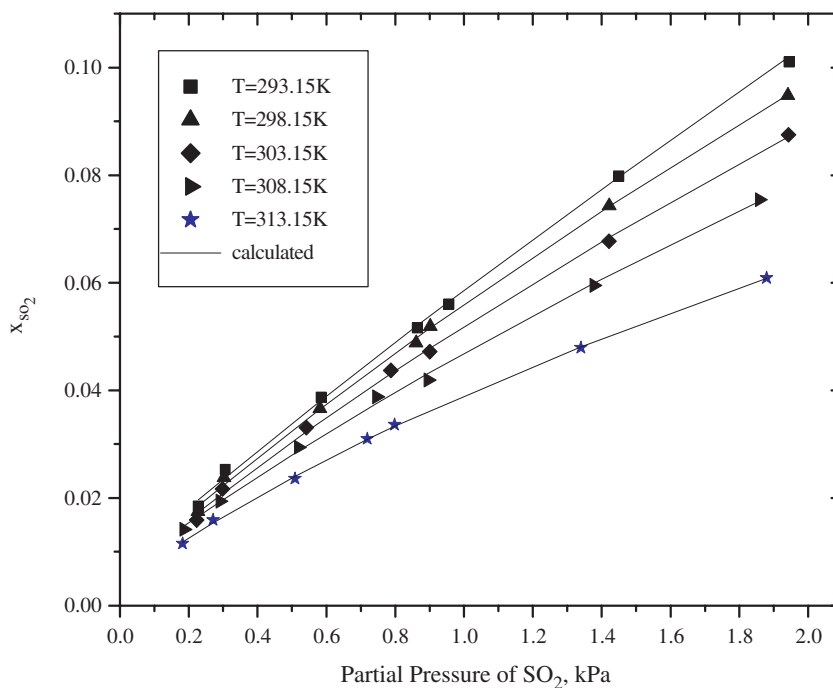
| System       | $\tau_{ij}$ |
|--------------|-------------|
| $SO_2$ -DMSO | 1.85        |
| DMSO- $SO_2$ | -4.35       |

Table 4. The parameters of substance.

| Substance   | $b_i$                   | Diameter $\sigma$ , Å | Stocks radius | Pauling radius |
|-------------|-------------------------|-----------------------|---------------|----------------|
| $SO_2$      | $3.938 \times 10^{-5}$  | 4.112 [15]            |               |                |
| DMSO        | $8.7055 \times 10^{-5}$ | 5.267 [15]            |               |                |
| $H^+$       | $5.4458 \times 10^{-7}$ | 1.20 [16]             | 0.73 Å        |                |
| $Mn^{2+}$   | $1.2909 \times 10^{-6}$ | 1.60 [16]             | 2.48 Å        |                |
| $SO_4^{2-}$ | $2.7771 \times 10^{-5}$ | 4.45 [16]             | 2.3 Å [22]    | 2.815 Å [22]   |

Table 5. The dependence of the dielectric constant of pure substance and temperature.

| Substance | Expression           | Temperature range, K | Source  |
|-----------|----------------------|----------------------|---------|
| $SO_2$    | $D = 36.67 - 0.077T$ | 287.15–373.15        | [23]    |
| DMSO      | $D = 91.21 - 0.15T$  | 293.15–328.15        | [23,24] |

Figure 1. The comparison of experimental data and calculation values for  $SO_2$  solubilities in mixture absorbent at different  $SO_2$  partial pressure.

### 3. Conclusion

1. According to the measured solubilities of dilute  $\text{SO}_2$  in  $\text{DMSO} + \text{Mn}^{2+}$  mixture solvent from 294.15 K to 313.15 K and partial pressure of  $\text{SO}_2$  from 0.41 kPa to 2.70 kPa, as well as a previous paper by Furst [1–3,17,20], a suitable electrolyte solution model based on gas–liquid phase equilibrium principles of electrolyte solution has been developed to present a gas–liquid equilibrium system, which takes into account interactions between ions and molecules or between cations and anions to the contribution of the Helmholtz energy, and takes into account the Helmholtz energy arising from the repulsive forces and the attractive forces between molecules through the improved SRK equation of state by Wang *et al.* [7,8].
2. From figure 1, we see that the solubilities calculated by the model are in good agreement with experimental data.
3. Compared with other models, this model is rather simple and applicable; the calculational accuracy is also satisfactory.
4. The experimental solubility and established EOS model in this work can be used as essential data and a model to improve the process design of removal of  $\text{SO}_2$  from flue gas.

### Nomenclature

|             |   |
|-------------|---|
| $A$         | Helmholtz free energy, $\text{J mol}^{-1}$                        |
| $a^{SR}$    | energy parameter  |
| $b$         | covolume, $\text{m}^3 \text{mol}^{-1}$                            |
| $D$         | dielectric constant   |
| $e$         | protonic charge, $1.60219 \times 10^{-19} \text{ C}$              |
| $g_{nm}$    | NRTL parameter  |
| $k_{ij}$    | binary parameter for Wong-Sandler mixing rule                     |
| $N$         | Avogadro constant, $6.022 \times 10^{23}$                         |
| $m_1 - m_3$ | parameter for equation of state                                   |
| $R$         | universal gas constant, $8.314 \text{ J mol}^{-1} \text{ K}^{-1}$ |
| $T$         | temperature, K  |
| $p$         | pressure, kPa   |
| $p_c$       | critical pressure   |
| $T_c$       | critical temperature  |
| $x$         | molar fraction  |
| $Z$         | ionic charge  |
| $v$         | molar volume, $\text{m}^3 \text{mol}^{-1}$                        |

### Greek letters

|                 |  |
|-----------------|--|
| $\Delta$        | difference   |
| $\Gamma$        | shielding parameter  |
| $\sigma$        | hard-sphere diameter   |
| $\omega$        | acentric factor  |
| $\zeta_3$       | packing factor   |
| $\varepsilon_0$ | electric permittivity of free space, $8.854188 \times 10^{-12} \text{ J}^{-2} \text{ C}^{-2} \text{ m}^{-1}$ |

|             |   |
|-------------|---|
| $\tau_{ij}$ | NRTL binary parameter                           |
| $\lambda$   | correlation parameters defined in equation (46) |

### Subscripts

|        |                             |
|--------|-----------------------------|
| a      | anion                       |
| c      | cation                      |
| $i, j$ | ionic species               |
| $k, l$ | ionic and molecular species |
| $n, m$ | molecular property          |
| SR     | short-range term            |
| LR     | long-range term             |
| 0      | standard properties         |

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